



Giornata di studio "Dispositivi di Sicurezza contro le sovrapressioni"

Standard di riferimento e normative applicabili

Principali omologazioni applicabili (CE e ASME): overview e principali differenze nell'iter omologativo

Ing. Fabio Rampini – PARCOL SpA

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AIS – ISA Italy Section Viale Campania, 31 – 20133 Milano Tel. 02 5412 3816 Email: ais@aisisa.it URL: www.aisisa.it ATI - Sezione Lombardia Via Giustiniano, 11 – 20133 Milano Tel. 02 784 989 Email: atilombardia@ati2000.it URL: www.ati2000.it



The world of pressure relief devices is actually dominated by American and European certifications, respectively known as "*ASME Stamp*" and "*CE marking*". The ASME Stamp certification follows the American Standards (ASME and API), the CE marking follows the International Standards under ISO/EN.

The American standards are well consolidated: the first issue and adoption of the ASME Code was in 1915; that one of the API 520 (at that time called "*recommended practice"*) is dated 1955.

The first issue of an ISO standard for pressure relief devices (ISO 4126 – General requirements) is dated 1981.

ASME code started up from the need to setting a standard to be followed by the rising industry. Large adoption also outside the United States is a consequence of its long history. ASME code is considered reliable and complete. If a subject is not exhaustively developed into the Code itself, the Code refers to other reference documents (for pressure relief devices, mainly API 520 and 526).

The standard EN 4126 comes from the converge of the original national standards and norms (BS, DIN, AFNOR, UNI, etc.) from the various European Countries. This convergence follows the constitution of the European Union and the issue of the several European Directives to be satisfied within the Union.

For pressure relief devices, the applicable Directive is the Pressure Equipment Directive 2014/68/UE (PED). Pressure relief devices are defined as safety accessories and classified in category IV.

The standard EN 4126 was initially developed in parallel with the standard ISO 4126. Since the European Working Group and International Working Group are mainly composed by the same experts, in the last years, the standard has been developed by Technical Committee ISO/TC 185 "Safety Devices for protection against excessive pressure" in collaboration with Technical Committee CEN/TC 69 "Industrial valves" the secretariat of which is held by AFNOR.







The current ISO international standard is identical to the corresponding EN ISO European standard, a part for the *Annex ZA* – *Relationship between this International Standard and the Essential Requirements of EU Directive*, not included in the published ISO.

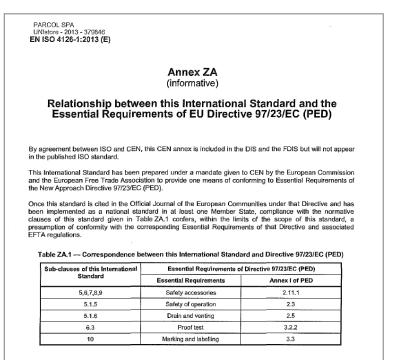
The parts of the European EN ISO standards are also called "*harmonized standards*", because, with the Annex ZA provide the compliance to the requirements (the so called "*essential safety requirements*"), that products shall satisfy to be CE marked. Note: the essential safety requirements refer to Materials, Design, Manufacturing, etc.

In the American world, everything is defined, regulated and written: valve overall dimensions, orifices size, mechanical design, valve sizing and selection, testing procedures and laboratories, etc. This means that the same pressure relief device certified ASME Stamp produced by two different manufacturers, passed the same technical prescriptions listed in the ASME Code.

In the European Union, the approach is different: every Manufacturer, within the rules defined in PED, can use the standards and design codes he prefers, but always giving evidence that the PED essential safety requirements are satisfied.

This means that, the same pressure relief device manufactured by two different Manufacturers for the same market (and, exasperating, for the same plant) should be different in one or more aspects. As an example, a Manufacturer will adopt American materials and design codes, the other one will choose European materials and design standards.

		ANNEX II
		CONFORMITY ASSESSMENT TABLES
1. Th	ie refe	rences in the tables to categories of modules are the following:
Ι	=	Module A
п	=	Modules A2, D1, E1
III	=	Modules B (design type) + D, B (design type) + F, B (production type) + E, B (production type) + C2, H
IV	=	Modules B (production type) + D, B (production type) + F, G, H1



WARNING: Other requirements and other EU Directives may be applicable to the products falling within the scope of this standard.

PARCOL Codes, standards and involved Organizations

				Compliance to ISO 17025			
		ASME Stamp	CE marking	- General requirements for the competence of			
Reference Codes and Standards		- ASME - API	 - ISO - EN - Nationals (for Italy: UNI) - Any accredited (e.g.: ASME, API) 	testing and calibration laboratories ISO/DIS 4126-11 requires that the laboratories test reports comply with the requirements of ISO 17025. This does not			
Involved Organizations	for Codes and standards	- ASME - API	- ISO/TC 185 - CEN - for Italy: CTI-UNI (CT 223/GL 01)	mean that a third party certifies it. The laboratory can check the accordance or if a third party (e.g., EU Notified Body) is involved, this can ask to evidence			
	for certification	- ASME - ASME certified *	- EU Notified Bodies °	the accordance. No certification is required.			
Testing laborato	ries	- ASME certified *	- Any accredited °				
	ndent inspectors and flow and Pressure Vessel Ins	w laboratory are from The pectors.					
° An Italian Notified Bod			ISO 4126-1:2013(E)	Bibliography			
			[1] ISO 6708:1995, Pipework component	nts — Definition and selection of DN (nominal size)			
6.6 Seat leakage test			[2] ISO 7268, Pipe components — Defin	nition of nominal pressure			
olo Seat leakage test			[3] ANSI/ASME B 16.34, Valves — Flan	nged, threaded, and welding end			

[3]

[4]

[5]

API 527, Seat tightness of pressure relief valves

EN 12516 (all parts), Industrial valves — Shell design strength

The seat leakage test of a safety valve shall be carried out after adjustment of the set or cold differential test pressure. The test procedure and leakage rate shall be agreed between the manufacturer and the purchaser

NOTE For example, API 527 can be used.

Reference Organizations – ASME Stamp General overview



ASME is a not-for-profit membership organization that enables collaboration, knowledge sharing, career enrichment, and skills development across all engineering disciplines, toward a goal of helping the global engineering community develop solutions to benefit lives and livelihoods. Founded in 1880 by a small group of leading industrialists, ASME has grown through the decades to include more than 130,000 members in 151 countries. Thirty-two thousand of these members are students.

From college students and early-career engineers to project managers, corporate executives, researchers and academic leaders, ASME's members are as diverse as the engineering community itself. ASME serves this wide-ranging technical community through quality programs in continuing education, training and professional development, codes and standards, research, conferences and publications, government relations and other forms of outreach.



The American Petroleum Institute (API) is the only national trade association that represents all aspects of America's oil and natural gas industry. Our 650 corporate members, from the largest major oil company to the smallest of independents, come from all segments of the industry. They are producers, refiners, suppliers, marketers, pipeline operators and marine transporters, as well as service and supply companies that support all segments of the industry.

Although our focus is primarily domestic, in recent years our work has expanded to include a growing international dimension, and today API is recognized around the world for its broad range of programs:

- Mission
- Advocacy
- Research & Statistics
- Standards
- Certification



nationalboard.org

The National Board of Boiler and Pressure Vessel Inspectors was created in 1919 to promote greater safety to life and property through uniformity in the construction, installation, repair, maintenance, and inspection of pressure equipment.

The National Board membership oversees adherence to laws, rules, and regulations relating to boilers and pressure vessels. The National Board Members are the chief boiler inspectors representing most states and all provinces of North America, as well as many major cities in the United States.

cen.eu

Reference Organizations – CE marking General overview



iso.org

ISO (the International Organization for Standardization) is a worldwide federation of national standards bodies (ISO member bodies). The work of preparing International Standards is normally carried out through ISO technical committees. Each member body interested in a subject for which a technical committee has been established has the right to be represented on that committee. International organizations, governmental and non-governmental in liaison with ISO, also take part in the work. ISO collaborates closely with the International Electrotechnical Commission (IEC) on all matters of electrotechnical standardization.

International Standards are drafted in accordance with the rules given in the ISO/IEC Directives, Part 2.

The main task of technical committees is to prepare International Standards. Draft International Standards adopted by the technical committees are circulated to the member bodies for voting. Publication as an International Standard requires approval by at least 75 % of the member bodies casting a vote. CEN, the European Committee for Standardization, is an association that brings together the National Standardization Bodies of 33 European countries.

CEN is one of three European Standardization Organizations (together with CENELEC and ETSI) that have been officially recognized by the European Union and by the European Free Trade Association (EFTA) as being responsible for developing and defining voluntary standards at European level.

CEN provides a platform for the development of European Standards and other technical documents in relation to various kinds of products, materials, services and processes. CEN supports standardization activities in relation to a wide range of fields and sectors including: air and space, chemicals, construction, consumer products, defence and security, energy, the environment, food and feed, health and safety, healthcare, ICT, machinery, materials, pressure equipment, services, smart living, transport and packaging.



uni.com

UNI - Ente Nazionale Italiano di Unificazione è un'associazione privata senza scopo di lucro riconosciuta dallo Stato e dall'Unione Europea che da quasi 100 anni elabora e pubblica norme tecniche volontarie – le norme UNI – in tutti i settori industriali, commerciali e del terziario.

Sono soci UNI le imprese, i professionisti, le associazioni, gli enti pubblici, i centri di ricerca, gli istituti scolastici e accademici, le rappresentanze dei consumatori e dei lavoratori, il terzo settore e le organizzazione non governative, che insieme costituiscono una piattaforma multi-stakeholder di confronto tecnico unica a livello nazionale.

UNI rappresenta l'Italia presso le organizzazioni di normazione europea (CEN) e mondiale (ISO) e organizza la partecipazione delle delegazioni nazionali ai lavori di normazione sovranazionale, con lo scopo di: - promuovere l'armonizzazione delle norme necessaria al funzionamento del mercato unico,

- sostenere e trasporre le peculiarità del modo di produrre italiano in specifiche tecniche che valorizzino l'esperienza e la tradizione produttiva nazionale.

Gruppo Misto CTI-UNI

COL

CT 223/GL 01 – Dispositivi di protezione e controllo degli impianti a pressione

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			ura delle diverse parti de aborazione la parte 2 e la			'ISO/TC 185. <mark>Di</mark> que	ste, la ISO 4126-6:2014 e	è l'ultima	

Reference Codes and Standards American Society of Mechanical Engineers (ASME)

ASME Boiler & Pressure Vessel Code (2015 Edition) is composed by 12 sections (see right). Sections related to pressure relief devices are:

- Section I Power Boilers (ovp 3%; bd 4%)
- Section II Materials
- Section V Nondestructive Examinations
- Section VIII Pressure vessels (ovp 10%; bd 7%)
- Section IX Welding

Other ASME related documents are:

- ASME B16.34 (2014) = Valves Flanges, Threaded and Welding End
- ASME B31.1 (2014) = Power piping
- ASME PTC-25 (2014) = Pressure relief devices *

* PTC stands for "Performance Test Code"

SECTIONS

I Rules for Construction of Power Boilers

II Materials

- Part A Ferrous Material Specifications
- Part B Nonferrous Material Specifications
- Part C Specifications for Welding Rods, Electrodes, and Filler Metals
- Part D Properties (Customary)
- Part D Properties (Metric)
- III Rules for Construction of Nuclear Facility Components
 - Subsection NCA General Requirements for Division 1 and Division 2
 - Appendices
 - Division 1
 - Subsection NB Class 1 Components
 - Subsection NC Class 2 Components
 - Subsection ND Class 3 Components
 - Subsection NE Class MC Components
 - Subsection NF -- Supports
 - Subsection NG Core Support Structures
 Subsection NH Class 1 Components in Elevated Temperature Service
 - Division 2 Code for Concrete Containments
 - Division 3 Containments for Transportation and Storage of Spent Nuclear Fuel and High Level Radioactive
 Material and Waste
 - Division 5 High Temperature Reactors
- IV Rules for Construction of Heating Boilers
- V Nondestructive Examination
- VI Recommended Rules for the Care and Operation of Heating Boilers
- VII Recommended Guidelines for the Care of Power Boilers
- VIII Rules for Construction of Pressure Vessels
 - Division 1
 - Division 2 Alternative Rules
 - Division 3 Alternative Rules for Construction of High Pressure Vessels
- IX Welding, Brazing, and Fusing Qualifications
- X Fiber-Reinforced Plastic Pressure Vessels
- XI Rules for Inservice Inspection of Nuclear Power Plant Components
- XII Rules for Construction and Continued Service of Transport Tanks

8

Reference Codes and Standards American Petroleum Institute (API)

- API STANDARD 520, Part I (2014) Sizing, Selection and Installation of Pressure-relieving Devices in Refineries – Sizing and selection
- API STANDARD 520, Part II (2015) Sizing, Selection and Installation of Pressure-relieving Devices in Refineries – Installation
- API STANDARD 521 (2014) Pressure-relieving and Depressurizing Systems
- API STANDARD 526 (2009) Flanged Steel Pressure-relief Valves
- API STANDARD 527 (2014) Seat tightness of Pressure-relief Valves

Cor	ntents			energ	
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			ng, Sala		Page
1	Scope	or pr	essur	tion, and In Plieving De ^{election}	Page Pstallation
		Part.	Sure-re	elia", and In	
2	Normative References	410	Sizin	"evina n	stallati
3	Normative References Terms and Definitions Pressure-relief Devices General Pressure-relief Valves (PRVs)	APION	Sizing and S	a De	Vices Vices
4	Pressure-relief Devices/	VINTHENDA	RD	election	
4.1	General	EDITI	ON 10		
4.2	Pressure-relief Valves (PRVs)		, SULY 2014		4
4.3	Rupture Disk Devices				2
4.4	Pin-actuated Devices			•••	
4.5	Open Flow Paths or Vents				44
4.6	Other Types of Devices				
5	Procedures for Sizing				
5.1	Determination of Relief Requirement	ts			
5.2	API Effective Area and Effective Co	efficient of [Discharge		
5.3	Backpressure				
5.4	Relieving Pressure				
5.5	Development of Sizing Equations				
5.6	Sizing for Gas or Vapor Relief				
5.7	Sizing for Steam Relief				
5.8	Sizing for Liquid Relief: PRVs Requi	• •	•		
5.9	Sizing for Liquid Relief: PRVs Not R				
	Sizing for Two-phase Liquid/Vapor F				
	Sizing for Rupture Disk Devices				
	Sizing for Open Flow Paths or Vents				
Ann	ex A (informative) Rupture Disk Devic	e Specificat	ion Sheet		
Ann	ex B (informative) Review of Flow Equ	ations Used	d in Sizing Pres	sure-relief Device	s 88
Ann	ex C (informative) Sizing for Two-phas	₃e Liquid∕Va	por Relief		
Ann	ex D (informative) Pressure-relief Valv	e Specificat	tion Sheets	• • • • • • • • • • • • • • • • • • • •	
Ann	ex E (informative) Capacity Evaluatior Constant Pipe Diameter			• •	
Bibl	liography				
Figu	Ires				
1	Conventional PRV with a Single Adj	usting Ring	for Blowdown	Control	
2	Balanced-bellows PRV				
3	Balanced-bellows PRV with an Auxi	liary Balanc	ed Piston		
4	Conventional PRV with Threaded Co				
5	PRV Operation-Vapor/Gas Service .				
6	Typical Relationship Between Lift of	Disk in a P	RV and Vessel I	Pressure	
7	PRV Operation-Liquid Service				

Typical Effects of Superimposed Backpressure on the Opening Pressure of Conventional PRVs 17

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Flange relief V			ress	sure-						Materia	als ^b	Valve Size	Fla	ME nge 2SS			(F	isig)	ssure Limit		Li	Pressure mit ^a sig)	Dimer	-to-Face nsions n.)
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	4N6 4N6	600 900	150 300		1200 1800	930 1395	600	9 ¹³ /16	9 ³ /16	pres	ssure limits	s are the d	esign pr	essure	of the bellow	/s at the ou	tlet tempera	ture of 100 °	e temperatu ºF, and pres	sure values	at other ten	nperatures n	nay be de	utlet terminec
	4N6	1500	300		3000	2330	600	9 ¹³ /16	9 ³ /16	from	n Annex C.	. User is ca	autioned	to revi	ew the outle	temperatu	re for possil	ole cryogeni	c application Other suitabl	is and selec	the approp	onate materi	als.	
B16.34. The or from Annex B ranges above i b Materials given	utiet Bange val or from tables i may not be line are minimum	ues at 100 °F n ASME B16. sar. User is ca requirements	above are the 34, if these va utioned to rev for the pressu	timit for this standa lues do not exceed iew the outlet temp are and temperature	ard. Inlet and outlet f I the values in paren erature for possible	lange pressure va theses or the outle cryogenic application	lues at other temperat et flange values at 100 lions and select the ap	n parentheses is less than that hree may only be interpolated b P above. Pressure changes of propriate materials. for the service involved.	using charts	c Set d Mate	lved. pressure li erials limite	imited for li ed to 900 °	ow-press F. Press	sure ap sure rat	plications wings indicate	here a class Id in the 100	s 300 inlet fi 00 °F colum		erred over a I to 900 °F.			, us roqui		-0.106

Reference Codes and Standards International Organization for Standardization (ISO)



ISO 4126 consists of the following parts, under the general title *Safety valves for protection against excessive pressure:*

- Part 1: Safety valves (2013)
- Part 2: Bursting discs safety devices (2003)
- Part 3: Safety valves and bursting disc safety devices in combination (2006)
- Part 4: Pilot operated safety valves (2013)
- Part 5: Controlled safety pressure relief systems (CSPRS) (2013)
- Part 6: Application, selection and installation of bursting disc safety devices (2014)
- Part 7: Common data (2013)
- Part 9: Application and installation of safety devices excluding stand-alone bursting disc safety devices (2008)
- Part 10: Sizing of safety valves for gas/liquid two-phase flow (2010)
- Part 11: Performance testing (under preparation; last ISO/DIS is dated 2014-08)

PARCOL PARCOL'S Spe Reference Organizations – CE marking

	INTERNATIONAL STANDARD	ISO 4126-1	EUROPEAN STANDARD EN K NORME EUROPÉENNE EUROPÄISCHE NORM July 201	3 4126-1	NORMA Europea	Dispositivi di sicurezza per la protezione contro l sovrapressioni Parte 1: Valvole di sicurezza	SETTEME
		Third edition 2013-07-15	ICS 13.240	Supersedes EN ISO 4128-1:2004			
			English Version			Safety devices for protection against excessive pressure Part 1: Safety valves	
			Safety devices for protection against exces 1: Safety valves (ISO 4126-1			La norma indica i requisiti generali per le valvole di sicu indipendentemente dal fluido per il quale sono state progetta Essa si applica alle valvole di sicurezza che hanno un clam	e. tro di
	Safety devices for protect excessive pressure —	tion against	Disposit/l's de sécurité pour pretoction contre les pressions Sicherhe excessives - Partie 1: Soupspus de sûnité (ISO 4126- 1:2013)	itseinrichtungen gegen unzulässigen Überdruck - eil 1: Sicherbeitsventile (ISO 4126-1:2013)		passaggio utilizzabile uguale o maggiore di 4 mm per press taratura di 0,1 bar o maggiori. Non è prevista nessuna limita per la temperatura.	oni di zione
	Part 1:		This European Standard was approved by CEN on 28 December 2012.				
	Safety valves		CEN members are bound to comply with the CEN/CENELEC Internal Regulations whic Standard the status of a national standard without any alteriation. Up-to-dete lists and bo standards may be obtained on application to the CEN-CENELEC Management Centre (PARCOL SPA			
	Dispositifs de sécurité pour protection contre l Partie 1: Soupapes de sûreté	les pressions excessives —	numbare may be obtained on appropriate in to be QueV_QUEVELTC. Nanagement Common This European Standard exists in three official vorsions (English, French, German). A v under the responsibility of a CEN member into its own language and notified to the CEP status as the official versions.	UNistore - 2013 - 379846 EN ISO 4126-1:2013 (E)			
			CEN members are the notional structure bodies of Austin, Beldam, Bulgeria, Dottal, Prietar, former Yugeria, Penalde of Macadani, Frience, Gennaue, Genes, Nangary, Lucenborg, Mala, Netherlands, Koney, Polend, Poligal, Romana, Slovata, Slove Kongdon.		Annex Za (informative		
		5				ational Standard and the Directive 97/23/EC (PED)	
		Reference number ISO 4126-12013(7)	BIRGHAR CRAMTER FOR FAILURE DIRECTION OF AND	in the published ISO standard. This International Standard has been and the European Free Trade Associ the New Approach Directive 97/23/EC Once this standard is cited in the Off been implemented as a national sta clauses of this standard given in Tr	prepared under a manc ation to provide one me (PED). cial Journal of the Euron dard in at least one able ZA.1 confers, with	uded in the DIS and the FDIS but will not appear date given to CEN by the European Commission aans of conforming to Essential Requirements of pean Communities under that Directive and has Member State, compliance with the normative in the limits of the scope of this standard, a Requirements of that Directive and associated	
	ISO	© ISO 2013		Table ZA.1 Correspondence b	etween this Internation	nal Standard and Directive 97/23/EC (PED)	
UNI EN ISO 4126-1:2013	2	\$ 130 2015	UNI EN ISO 4126-1:2013	Sub-clauses of this International	Essential Requi	irements of Directive 97/23/EC (PED)	
				Standard	Essential Requirem	nents Annex I of PED	
				5,6,7,8,9	Safety accessorie	es 2.11.1	
				5.1.5	Safety of operation	on 2.3	
				5.1.6	Drain and ventin	g 2.5	
				6.3	Proof test	3.2.2	
				10	Marking and labelli	ing 3.3	

Steps for certification of safety valves

RCOL

ASME UV Stamp (ASME Sect. VIII Div. 1) vs. CE marking (ISO 4126-1)

. Application Form	1. Application Form
The Manufacturer contacts ASME. . Design review The technical dossier for the product/series under certification is reviewed by ASME or ASME certified inspector.	The Manufacturer contacts the selected Notified Body. 2. Design review The technical dossier for the product/series under certification is reviewed by the Notified Body.
• Initial Certification Testing ("Provisional Testing") The selected ASME certified flow laboratory defines the number of sample to be tested to define the performance characteristics of the product/series (overpressure, coefficient of discharge, blowdown).	3. Performance Testing The Manufacturer and the Notified Body select the accredited flow laboratory and the number of sample to be tested to define the performance characteristics of the product/series (overpressure, coefficient of discharge, blowdown).
. Quality System Review Performed at Manufacturer's facilities. The ASME Quality Manual supplied by the Manufacturer is reviewed and approved.	 4. Quality System Review Performed at Manufacturer's facilities. The ISO Quality Manual supplied by the Manufacturer is reviewed and approved.
 Production Certification Testing During Quality System Review, the ASME Inspector selects the valves to be tested at the ASME certified flow laboratory. Valves are assembled and tested (set pressure and leakage tests only) at Manufacturer's facilities under the ASME Inspector witnessing. 	 5. Production Certification Testing Part of the Quality System Review consists in the assembling and testing (hydrostatic pressure, set pressure and leakage tests) under the Notified Body Inspector witnessing. 6. Issuance of Certifications and Certificates
After plumbing, valves are shipped to the selected ASME certified flow laboratory to confirm the performances defined during Initial Certification Testing.	ASME O 4 8 12 16 20 2 Application form
. Issuance of Certifications and Certificates	Design review Initial Certification Testing Quality system review
	Production certification testing





Table of Contents



National Board Pressure Relief Device Certifications

NB-18

FOREWARD	1
NATIONAL BOARD PRESSURE RELIEF DEVICE CERTIFICATION	2
DETERMINATION OF CERTIFIED RELIEVING CAPACITIES	6
LISTING OF ASSEMBLER AND MANUFACTURER CERTIFICATIONS	11
LISTING OF CERTIFIED DEVICE TYPES	112
LISTING OF RUPTURE CCFs BY VALVE MANUFACTURER	671
LISTING OF VR CERTIFICATE HOLDERS	697

http://www.nationalboard.org/SiteDocuments/NB18/NB18.pdf

Stamps ASME (left) and National Board (right)

ASME Stamp Certified individual (CI)

ASME BPVC.VIII.1-2015

UG-116 - UG-117

UG-117 CERTIFICATES OF AUTHORIZATION AND CERTIFICATION MARKS

(a) A Certificate of Authorization to use the Certification Mark with the U, UM, UV, or UD Designators shown in Figures UG-116, UG-129.1, and UG-129.2 will be granted by the Society pursuant to the provisions of the following paragraphs. Stamps for applying the Certification Mark shall be obtained from the Society. For those items to be marked with the UM, UV, or UD Designators, a Certified Individual meeting the current requirements of ASME QAI-1 shall provide oversight to ensure that each use of the UM, UV, or UD Designators is in accordance with the requirements of this Division. In addition, each use of the UM, UV, or UD Designators is to be documented on the Certificate of Compliance Form (U-3 or U-3A) for vessels bearing the UM Designator, or a Certificate of Conformance Form (UV-1 or UD-1) as appropriate.

(1) Requirements for the Certified Individual (Cl). The CI shall:

(-a) be an employee of the Manufacturer or Assembler.

(-b) be qualified and certified by the Manufacturer or Assembler. Qualifications shall include as a minimum:

(-1) knowledge of the requirements of this Division for the application of the Certification Mark with the appropriate designator;

(-2) knowledge of the Manufacturer's or Assembler's quality program;

(-3) training commensurate with the scope, complexity, or special nature of the activities to which oversight is to be provided.

(-c) have a record, maintained and certified by the Manufacturer or Assembler, containing objective evidence of the qualifications of the CI and the training program provided.

(2) Duties of the Certified Individual (CI). The CI shall:

(-a) verify that each item to which the Certification Mark is applied meets all applicable requirements of this Division and has a current capacity certification for the "UV" or "UD" Designators;

(-b) for the "UV" or "UD" Designators, review documentation for each lot of items to be stamped to verify, for the lot, that requirements of this Division have been completed;

(-c) sign the appropriate Certificate of Compliance/Conformance Form U-3, U-3A, UV-1, or UD-1 as appropriate prior to release of control of the item.

(3) Certificate of Compliance/Conformance Form U-3, U-3A, UV-1, or UD-1.

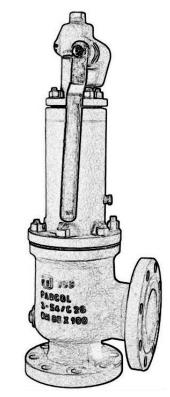
(-a) The appropriate Certificate of Conformance shall be filled out by the Manufacturer or Assembler and signed by the Certified Individual. Mass produced pressure relief devices may be recorded on a single entry provided the devices are identical and produced in the same lot.

(-b) The Manufacturer's or Assembler's written quality control program shall include requirements for completion of Certificates of Conformance forms and retention by the Manufacturer or Assembler for a minimum of five years.

(b) Application for Authorization. Any organization desiring a Certificate of Authorization shall apply to the Boiler and Pressure Vessel Committee of the Society, on forms issued by the Society, ⁴⁰ specifying the Certification Designator desired and the scope of Code activities to be performed. When an organization intends to build Code items in plants in more than one geographical area, either separate applications for each plant or a single application listing the addresses of all such plants may be submitted. Each application shall identify the Authorized Inspection Agency providing Code inspection at each









Terms and definitions

Reference stan	dard	API 520 Part 1 (2014)	ISO 4126-1:2013
set pressure	pset	The inlet gauge pressure at which the pressure relief device is set to open under service conditions	Predetermined pressure at which a safety valve under operating conditions commences to open (1)
overpressure	ovp	The pressure increase over the set pressure of the relieving device. Overpressure is expressed in pressure units or as a percentage of set pressure. Overpressure is the same as accumulation only when the relieving device is set to open at the maximum allowable working pressure of the vessel	Pressure increase over the set pressure (2)
coefficient of discharge	к	The ratio of the mass flow rate in a valve to that of an ideal nozzle. The coefficient of discharge is used for calculating flow through a pressure relief device	Value of actual flowing capacity (from tests) divided by the theoretical flowing capacity (from calculation)
blowdown	bd	The difference between the set pressure and the closing pressure of a pressure relief valve, expressed as a percentage of the set pressure or in pressure units	Difference between set and reseating pressures (3)
back pressure	bp	The pressure that exists at the outlet of a pressure relief device as a result of the pressure in the discharge system. Backpressure is the sum of the superimposed and built-up backpressures. built-up backpressure The increase in pressure at the outlet of a pressure relief device that develops as a result of flow after the pressure relief device opens. superimposed backpressure The static pressure that exists at the outlet of a pressure relief device at the time the device is required to operate. Superimposed backpressure is the result of pressure in the discharge system coming from other sources and may be constant or variable.	Pressure that exists at the outlet of a safety valve as a result of the pressure in the discharge system (4) built-up back pressure Pressure existing at the outlet of a safety valve caused by flow through the valve and the discharge system superimposed back pressure Pressure existing at the outlet of a safety valve at the time when the device is required to operate
flow area	A	Actual discharge area The area of a pressure relief valve (PRV) is the minimum net area that determines the flow through a valve	Minimum cross-sectional flow area (but not the smallest area between disc and seat) between inlet and seat which is used to calculate the theoretical flow capacity, with no deduction for any obstruction

1) It is the gauge pressure measured at the valve inlet at which the pressure forces tending to open the valve for the specific service conditions are in equilibrium with the forces retaining the valve disc on its seat

2) Overpressure is usually expressed as a percentage of the set pressure

3) Blowdown is normally stated as a percentage of set pressure except for pressures of less than 3 bar when the blow down is expressed in bar

4) The back pressure is the sum of the superimposed and built-up back pressures

Typical PRV functional characteristics

Reference standard	1	API 520 Pa	art 1 (2014)	ISO 4126-1:2013			
service		vapor/gas	liquid	vapor/gas	liquid		
max overpressure	ovp	10% ÷ 21%	10% ÷ 25%	10%	10%		
coefficient of discharge	к	0.975 (1)	0.37 ÷ 0.62 (1)	-	-		
max blowdown	bd	15% (1)	15% (1)	15%	20%		
max back pressure	bp	50% (1) (2)	50% (1) (2)	(3) (4)	(5)		

1) For reference only. Refer to PRV manufacturer for effective value.

2) Evaluated as bp / pset | gauge (50% is valid for balanced valves only; for conventional ones, consider 10%)

- 3) No indication, but tests shall be performed for backpressures higher than 25%
- 4) Evaluated as bp / (pset + ovp) | abs
- 5) Evaluated as bp / (pset + ovp) | gauge according to ISO/DIS 4126-11 Safety devices for protection against excessive pressure Part 11: Performance testing



API STANDARD 520, PART 1—SIZING AND SELECTION SIZING, SELECTION, AND INSTALLATION OF PRESSURE-RELIEVING DEVICES IN REFINERIES

NOTE The curve above shows that up to and including 25 % overpressure, capacity is affected by the change in lift, the change in the orifice discharge coefficient, and the change in overpressure. Above 25 %, capacity is affected only by the change in overpressure. Noncertified valves operating at low overpressure tend to chatter; therefore, overpressures of less than 10 % should be avoided.

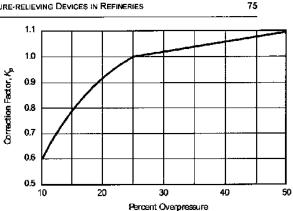


Figure 38—Capacity Correction Factors Due to Overpressure for Noncertified PRVs In Liquid Service



Reference standard	API 520 Part 1 (2014)	ISO 4126-7:2013
Vapor/Gas	$A_g = \frac{W}{CK_d P_1 K_b K_c} \sqrt{\frac{TZ}{M}}$	$A_g = \frac{Q_m}{p_0 C K_{dr} K_b} \sqrt{\frac{T_0 Z}{M}}$
Liquid	$A_{l} = \frac{11.78Q}{K_{d}K_{w}K_{c}K_{v}} \sqrt{\frac{\rho_{l}}{P_{1} - P_{2}}}$	$A_l = \frac{Q_m}{1.61K_{dr}K_{\nu}} \sqrt{\frac{\nu}{p_0 - p_b}}$
Alternate discharge	$A = \max\left(A_g; A_l\right)$	$A = \max\left(A_g; A_l\right)$
Two-phase mixture	$A_{C.2.2} = \frac{277.8W}{K_d K_b K_c K_v G}$ $A_{C.2.3} = \frac{16.67Q\rho_{l0}}{K_d K_b K_c K_v G}$	$ISO \ 4126-10:2010$ $A_{0} = \frac{Q_{m,out}}{K_{dr,2ph}C} \sqrt{\frac{\nu_{0}}{2p_{0}}}$

Note: refer to reference standards for proper terminology and units of measure

K _{dr}	Certified derated discharge coefficient. K _d is the coefficient of discharge <u>determined by test</u>	$= 0.9 \cdot K_d$
K _{dr,2ph}	Discharge coefficient for two-phase flow, <u>if not experimentally available</u> . $K_{dr,g}$, $K_{dr,l}$ and ϵ_{seat} are respectively the certified discharge coefficient for single-phase vapor/gas flow, the certified discharge coefficient for single-phase liquid flow and the void fraction in the narro west cross-section of the valve at sizing conditions for a homogeneous two-phase mixture	$= \varepsilon_{seat} \cdot K_{dr,g} + (1 - \varepsilon_{seat}) \cdot K_{dr,l}$

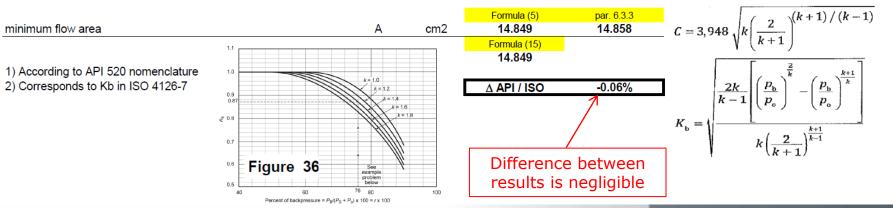
Valve sizing Gas – Critical flow

COL

			API 520-1	ISO 4126-7	API
			2014	2013	critical
set pressure	pset	barg	10	10	
overpressure	ovp	%	10%	10%	$A = \frac{W}{CK_d P_1 K_b K_c} \sqrt{\frac{TZ}{M}} $ (5)
relieving pressure	p0	bar	12.01	12.01	$- CK_d P_1 K_b K_c \sqrt{M}$
relieving temperature	TO	°C	30	30	-
backpressure	pb	barg	0	0	$C = 0.03948 \sqrt{k \left(\frac{2}{k+1}\right)^{\frac{(k+1)}{(k-1)}}} $ (9)
flowrate	Q	kg/h	10 000	10 000	$C = 0.03948 \left k \left(\frac{2}{k} \right)^{(k-1)} \right $ (9)
					$\sqrt{(k+1)}$
molar mass	М	-	28.964	28.964	
compressibility factor	Z	-	1	1	-
isentropic exponent at relieving pressure and temperature	k	-	1.4	1.4	-
function of the isentropic exponent, k	С	-	0.0270	2.7033	-
					-
coefficient of discharge	Kd (1)	-	0.975	0.975	ISO
capacity correction factor due to backpressure	Kb (1)	-	1.000	1.000	
combination correction factor for installation with a rupture disc	Kc	-	1	1	. <u>M</u>
					$\dot{Q}_{\rm m} = p_{\rm o} CA K_{\rm dr} K_{\rm b} \sqrt{\frac{M}{ZT_{\rm o}}}$
backpressure ratio pb / p0 abs	r	-	8.4%	8.4%	$V_{\rm a} = V_{\rm a} = V_{\rm a}$
backpressure ratio pb / pset gauge	r_g	-	0%	0%	
critical pressure	рс	bar	6.35	6.35	C = 3,948 $\sqrt{k\left(\frac{2}{k+1}\right)^{(k+1)/(k-1)}}$
flux		-	critical	critical	$C = 3,948 \sqrt{ k \frac{2}{1+1}}$
					γ ($k+1$)
			Formula (5)	par. 6.3.3	
minimum flow area	A	cm2	11.350	11.352	_
					_
1) According to API 520 nomenclature			∆ API / ISO	-0.02%	
				K	-
				\sim	
				\setminus	
Flow is critical when $pb < pc$					\mathbf{X}
				Differen	
$k = \frac{k}{1-k}$					ce between
$p_c = p_0 \left[\frac{2}{k+1} \right]^{\frac{k}{k-1}}$				results i	s negligible
$p_c - p_0 \left[\frac{k+1}{k+1} \right]$				L	
rv ± 11					

Valve sizing Gas – Subcritical flow

			API 520-1	ISO 4126-7	API	
			2014	2013	critical	
set pressure	pset	barg	10	10	W = TZ	
overpressure	ovp	%	10%	10%	$- A = \frac{W}{CK_d P_1 K_b K_c} \sqrt{\frac{TZ}{M}} $ (5)	
relieving pressure	p0	bar	12.01	12.01		
relieving temperature	Т0	°C	30	30	(4+1)	
backpressure (superimposed, constant)	pb	barg	9	9	$C = 0.03948 \int k \left(\frac{2}{2}\right)^{\frac{(k+1)}{(k-1)}} $ (9)	
flowrate	Q	kg/h	10 000	10 000	$C = 0.03948 \sqrt{k \left(\frac{2}{k+1}\right)^{\frac{(k+1)}{(k-1)}}}$ (9)	
molar mass	М	-	28.964	28.964		
compressibility factor	Z	-	1	1	subcritical	
isentropic exponent at relieving pressure and temperature	k	-	1.4	1.4	$170 \times W$ $7T$	
function of the isentropic exponent, k	С	-	0.0270	2.7033	$- A = \frac{17.9 \times W}{F_2 K_d K_c} \sqrt{\frac{ZT}{M \times P_1 (P_1 - P_2)}} $ (*	15)
coefficient of discharge	Kd (1)	-	0.975	0.975		
capacity correction factor due to backpressure (Fig. 36)	Kb (1)	-	0.764	1.000		
combination correction factor for installation with a rupture disc	Kc	-	1	1	$F_{2} = \left \left(\frac{\kappa}{L-1} \right) r^{(k)} \right \frac{1-r}{1-r} \right $ (1)	18)
backpressure ratio pb / p0 abs	r	-	83.4%	05.470	$F_{2} = \sqrt{\left(\frac{k}{k-1}\right)r^{\binom{2}{k}}\left[\frac{1-r^{\binom{k-1}{k}}}{1-r}\right]} $ (1)	
backpressure ratio pb / pset gauge	r_g	-	90%	90%	-	
critical pressure	рс	bar	6.35	6.35	ISO	
flux		-	subcritical	subcritical	<u>M</u>	
capacity correction factor for subcritical flow (API)	F2	-	0.906	n.a.	$Q_{\rm m} = p_{\rm o} CA K_{\rm dr} K_{\rm b} \sqrt{\frac{m}{\pi m}}$	
theoretical capacity correction factor for subcritical flow (ISO)	Ksub (2)	-	n.a.	0.764	$\dot{Q}_{\rm m} = p_{\rm o} CA K_{\rm dr} K_{\rm b} \sqrt{\frac{M}{ZT_{\rm o}}}$	



Valve sizing Gas – Subcritical flow – F₂ and K_b

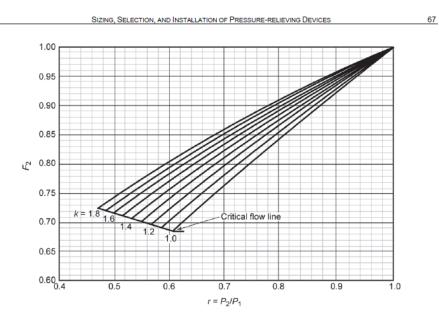
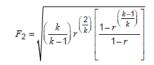


Figure 35—Values for F2 for Subcritical Flow

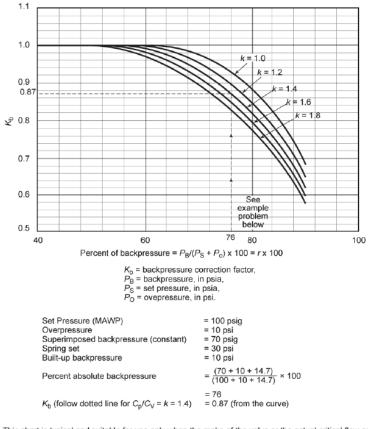


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(18)

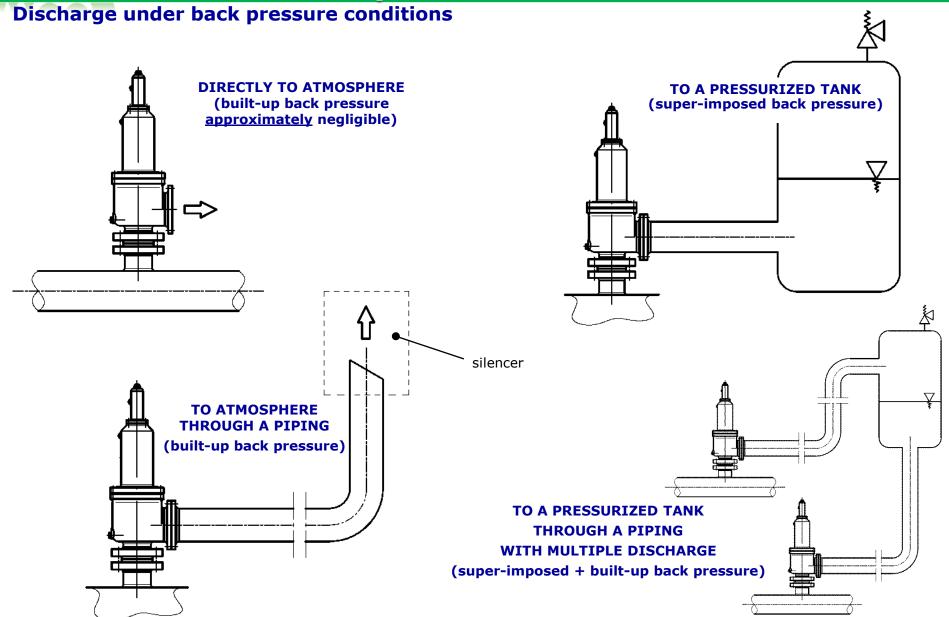
API STANDARD 520, PART I—SIZING AND SELECTION

5.6.4) equal to the critical flow equation (see 5.6.3) and algebraically solving for $K_{\rm b}$. A graphical presentation of the capacity correction factor, $K_{\rm b}$, is given in Figure 36. This alternate sizing procedure allows the designer to use the critical flow equation to calculate the same area obtained with the subcritical flow equation provided $K_{\rm b}$ is obtained from Figure 36 (instead of a $K_{\rm b}$ value of 1.0 when the critical flow equations of 5.6.3 are used).



NOTE This chart is typical and suitable for use only when the make of the valve or the actual critical flow pressure point for the vapor or gas is unknown; otherwise, the valve manufacturer should be consulted for specific data. This correction factor should be used only in the sizing of conventional (non-balanced) PRVs that have their spring setting adjusted to compensate for the superimposed backpressure. It should not be used to size balanced type valves.

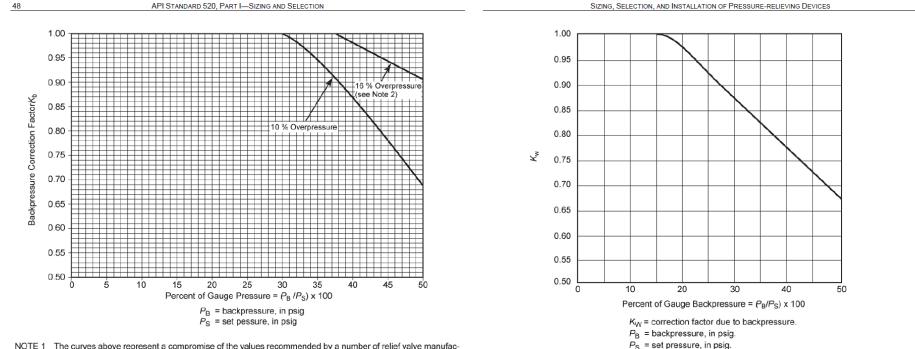
Figure 36—Constant Backpressure Correction Factor, *K*_b, for Conventional PRVs (Vapors and Gases Only)



Back pressure correction factors (API 520 Part 1)

Note : The curves are a compromise of the values recommended by various PRV manufacturers and may be used for a preliminary sizing only. **PRV manufacturers should be consulted for the effective correction factors**.

SHALL /



- NOTE 1 The curves above represent a compromise of the values recommended by a number of relief valve manufacturers and may be used when the make of the valve or the critical flow pressure point for the vapor or gas is unknown. When the make of the valve is known, the manufacturer should be consulted for the correction factor. These curves are for set pressures of 50 psig and above. They are limited to back pressure below critical flow pressure for a given set pressure. For set pressures below 50 psig or for subcritical flow, the manufacturer must be consulted for values of *K*_b
- NOTE 2 See 5.3.3.
- NOTE 3 For 21 % overpressure, K_b equals 1.0 up to $P_B/P_S = 50$ %.

Figure 30—Backpressure Correction Factor, K_b, for Balance Spring-loaded PRV (Vapors and Gases)

Milan, Sept. 21st – Giornata di Studio Dispositivi di Sicurezza ATI Lombardia

NOTE The curve above represents values above recommended by various manufacturers.

Figure 31—Capacity Correction Factor, K_w, Due to Backpressure on Balanced Spring-loaded

PRVs in Liquid Service

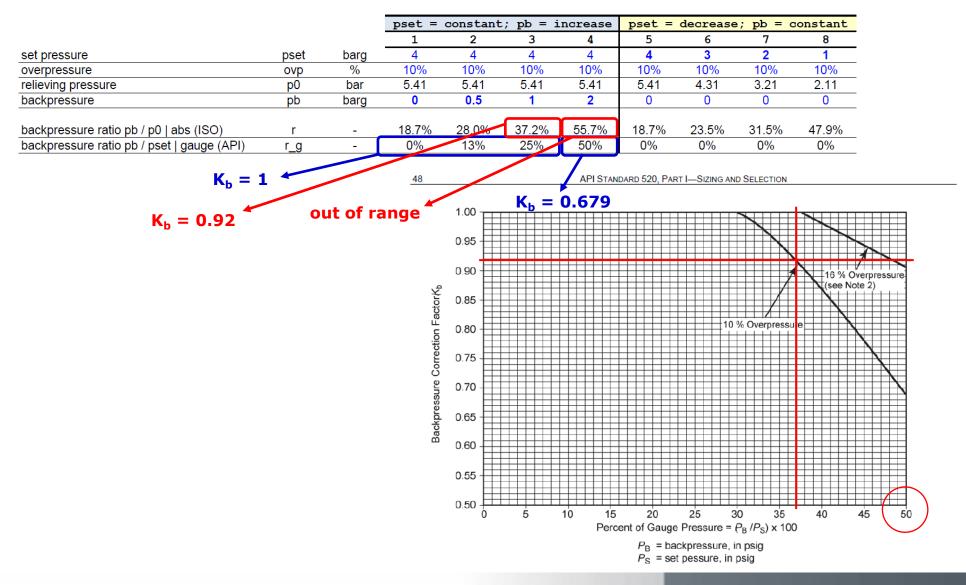
manufacturer should be consulted for the applicable correction factor.

This curve may be used when the manufacturer is not known. Otherwise, the

49

Valve sizing Gas – Evaluation of backpressure (API vs. ISO)

PARCO



Evaluation of back pressure Compressible vs. incompressible fluids

ISO 4126-1:2013 Par. 7.3.3.4 Value of test pressure

<<...For **compressible fluids** when the ratio of absolute back pressure to absolute relieving pressure exceeds the value of 0.25, the coefficient of discharge can be largely dependent upon this ratio. Then tests shall be conducted at ratios between the pressure ratio of 0.25 and the maximum pressure ratio required to obtain curves or tables of coefficient of discharge versus the ratio of absolute back pressure and absolute relieving pressure, this curve may be extended to cover the tests with pressure ratios less than 0.25. ...>>

ISO/DIS 4126-11:2011 Par. 3 Terms and definitions

- preliminary draft

Back pressure ratio (BPR)

The back pressure ratio is the ratio of back pressure and actual relieving pressure, usually expressed as percentage. Both definitions of BPR, based on gauge or absolute pressures, can be adopted for the purpose of tracing the curve of discharge coefficient vs. BPR.

If BPR is assumed as the ratio of absolute back pressure and actual absolute relieving pressure, the value of BPR is always equal to 100 when the back pressure equals the relieving pressure.

If BPR is defined as the ratio of back pressure and actual back pressure, both expressed as gauge, BPR is always null under atmospheric back pressure conditions, and equals 100 when the back pressure equals the relieving pressure.

Note: This definition of back pressure ratio modifies the one reported in the reference standards - e.g., 4126-1 § 7.3.3.4 - that refers to pressure in absolute units.

This difference/chance is related to the following reasons:

In the case of incompressible fluids, the parameter, accounting for the discharging flow rate, is the pressure difference rather than the absolute pressure ratio, as occurs in the case of compressible fluids. Moreover, the limiting ratio of Pb/Pp<0.25, expressed in absolute units, reported in 4126-1 § 7.3.3.4, lacks of meaning operating with incompressible fluids (as its origin is related to the passage from sonic to subsonic discharge conditions occurring in compressible fluids). Considering what above, it is clear that the operational and discharge capability of a safety valve operating with uncompressible fluids must be verified also for back pressure ratios less than 0.25
The main influence of back pressure is the lift reduction, that leads to the reduction of the discharge coefficient (mostly for geometrical reasons). In the case of a safety device operating with air at a low set pressure rate (i.e., closed to atmosphere), the BPR evaluated by absolute pressures can be very high also at atmospheric back pressure (50% for a relative relieving pressure of 1 bar) while the disc reaches the nominal lift. This implies that it can result quit hard to find a single curve representative of the K vs BPR trend for a valve size range also including low set pressures. The use of relative pressure in the definition of BPR can really help in finding this curve. Notice that the difference in the two definitions becomes negligible over a certain relieving pressure.

Testing laboratories Independent flow laboratories

The main area of the National Board Testing Laboratory contains three test systems using steam, nitrogen, and water. Each system features the following:

	Steam	Air			Water
Media	Dry Saturated Steam	Compressed Nitrogen			Ambient Temp. Water
Maximum Source Pressure	850 psi (58 bar)	3,500 psi (238 bar)			625 psi (43 bar)
Flow Measurement Method	Timed Weight Method	Sonic Flow Nozzle and Sharp-Edged Orifice Plate			Sharp-Edged Orifice Plates and Timed Weight Method
Maximum Stamped Set Pressure	500 psi (34 bar) 4" (DN 100)	Low 580 psi (39 bar) 6" (DN 150)	<u>Medium</u> 1,100 psi (75 bar) 4" (DN 100)	High 2,025 psi (138 bar) ³ ⁄4" (DN 20)	500 psi (34 bar) 4" (DN 100)
Maximum Stamped Flow Capacity	16,000 pph (7,257 Kg/h)	13,000 SCFM (22,087 m ³ /h)	25,000 SCFM (42,475 m ³ /h)	5,000 SCFM (8,495 m ³ /h)	550 gpm (2,082 L/min)



NATIONAL BOARD OF BOILER AND PRESSURE VESSEL INSPECTORS

<<... As the world's only independent ASME certified flow laboratory, the National Board Testing Laboratory, located north of Columbus, remains the leader in promoting accurate performance measurement of pressure relieving devices and the development of technical standards...>>

In April 2016, **Mr. Joseph Ball**, Director of National Bard Pressure Relief Department was nominated Convenor of ISO TC 185 WG 18 for the development of ISO 4126 Part 11: Performance Testing. Previous Convenor was **Prof. Vincenzo Dossena**, Head of

Fluid-dynamics of Turbo-machines Laboratories (LFM) at Politecnico di Milano University, that resigned in October 2015 after more than five years of important job culminating in the ISO/DIS 4126:11 dated 08-2014.

Media		air (dried and preheated)	water	
Media testing	temperature	ambient	ambient	
Valves inlet range		low pressure: $1/4'' \div 6''$ high pressure: $1/4'' \div 4''$	1/4" ÷ 3"	
Nozzle diamet	er	6 ÷ 70 mm	6 ÷ 50 mm	
Maximum Testing Pressure		35 bar	10 bar	
built-up		10 bar	10 bar	
Backpressure	superimposed	8 bar	6 bar	
Flow capacity		0.05÷8 kg/s	1÷80 kg/s	
Flow measurement method		sonic flow nozzle and sharp-edged orifice plate	electromagnetic flow-meter	

"Eluid-dynamics of Turbo-machines" Laboratories (LEM)



POLITECNICO DI MILANO

<<... Independent Testing Laboratory located in Milan, north of Italy, is leader in performance measurement of pressure relieving devices under backpressure conditions and the development of technical standards. It is the reference Testing Laboratory for Italian Manufacturers of pressure relieving devices. ...>>

Testing laboratories – NATIONAL BOARD (NBTL)

Parcol Safety Valves during Provisional Tests at "National Board Testing Laboratories" in Worthington, Columbus, OH



Testing laboratories – Politecnico di Milano (LFM)

PARCOL

Parcol Pressure Safety Relief Valves during Discharge Test at "Fluid-dynamics of Turbo-machines" Laboratories (LFM) at "Politecnico di Milano" University



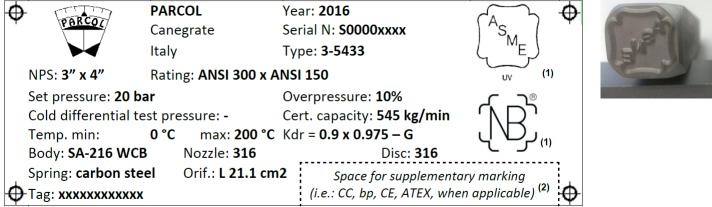
Required marking on identification plate

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ASME VIII-1	ISO 4126-1	PED
 the name of the manufacturer; manufacturer's design or type number; NPS size (DN) (the nominal pipe size of the valve inlet); set pressure, and, if applicable, cold differential test pressure; certified capacity (as applicable): kg/h of saturated steam at an overpressure of 10% or 0.2 bar, whichever is greater <u>for valves certified on steam;</u> I/min of water at 20°C at an overpressure of 10% or 0.2 bar, whichever is greater <u>for valves certified on steam;</u> kg/min of air at an overpressure of 10% or 0.2 bar, whichever is greater <u>for valves certified on water;</u> kg/min of air at an overpressure of 10% or 0.2 bar, whichever is greater for valves <u>on compressible fluids other than steam</u>. year built; the Certification Mark with the UV Designator placed under the Mark; the National Board Mark (valves series certified at National Board Testing Laboratories only). 	 set pressure in barg (or other internationally recognized unit); reference standard (ISO 4126-1:2013); manufacturer's series/type identification number; certified derated discharge coefficient (K_{dr}), indicating the reference fluid (<i>G</i> for gas, <i>S</i> for steam, <i>L</i> for liquid). Example: 0.9 x 0.945 - S; flow area in square millimetres (or other internationally recognized unit); lift minimum value, expressed in mm, and related overpressure (expressed, for example in percentage of set pressure); cold differential test pressure (if applicable) in barg (or other internationally recognized unit); serial number or alternative coding to indicate year of manufacture. 	 CE marking and identification code of Notified Body certifying the PED applied Module; the manufacturer name and its address or other means of identification of the manufacturer; year of manufacture; valve type or series; serial number; temperature <i>minimum</i> values: those mentioned within the classes of materials (e.g.: -20°C for C steel, +20°C for CrMo steel etc.) or defined by Technical Dept. for Client's specific applications; pressure and temperature <i>maximum</i> values: in case of no more limiting conditions than those defined by materials rating of pressure containing parts, the indication of rating and manufacture material is adequate; in case of more limiting conditions, due for example to the presence of non- metallic materials, their pressure and/or temperature maximum limits shall be defined; for example, the maximum temperature assuring the seals integrity shall to be indicated.

Typical identification plates

Typical for ASME Stamp





1) Marking by punching

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2) CC = ASME Code Case; supplementary requirements by Client, if any (e.g.: bp = backpressure)

Example: application of Code Case 2203

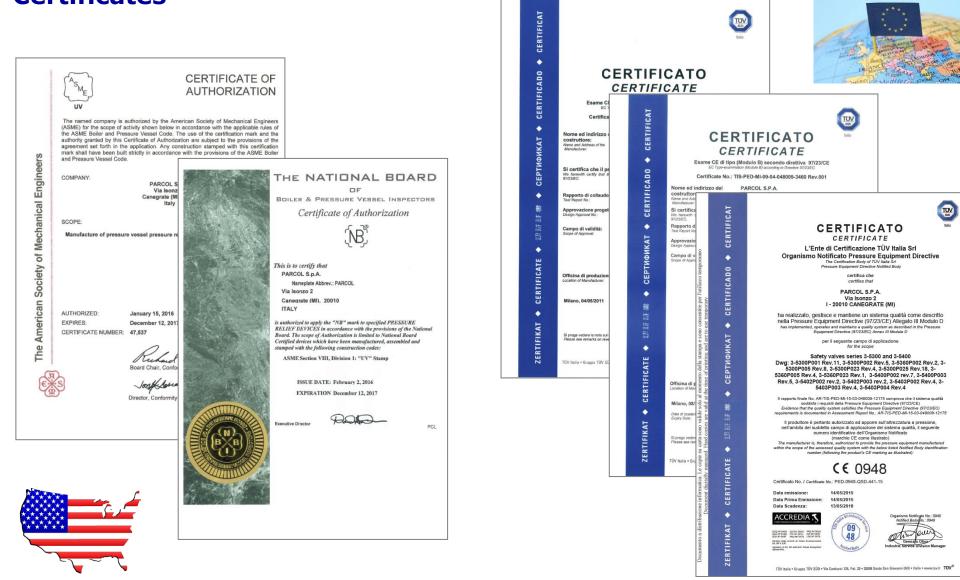
Lifting lever is mandatory on air, water over 60 °C and steam service. According to Code Case 2203, lifting lever can not be provided, but only with written approval by Customer. Reference to Code Case shall be present on valve identification plate.

PARCOL Year: 2016 Ф Ð Canegrate Serial N: S0000xxxx Italy Type: 3-5433 NPS: 3" x 4" Rating: ANSI 300 x ANSI 150 Overpressure: 10% Set pressure: 20 bar Cold differential test pressure: -Cert. capacity: 32 710 kg/h Kdr = 0.9 x 0.967 – G Temp. min: 0°C max: 200 °C Body: SA-216 WCB Nozzle: **316** Disc: **316** Spring: carbon steel Orif.: L 21.1 cm2 I 2 G T6X Tag: xxxxxxxxxxxx

Typical for CE and ATEX marking

1) Identification code of Notified Body certifying the Module D or the Module F







Many thanks for Your kind attention

fabio.rampini@parcol.com

Engineering and Development

Parcol S.p.A. Italy – 20010 Canegrate (MI) Via Isonzo, 2 Ph.+39 0331 413111 Fax +39 0331 404215 sales@parcol.com